Trayler, C.R., and Koczot, K.M., 1995, Regional Water Table (1994) and Water-Level Changes in the Morongo Basin, San Bernardino County, California

INTRODUCTION

The Morongo Basin is in the Mojave Desert region of southern California, about 100 mi east of Los Angeles. Ground water is virtually the sole source of water in the Morongo Basin. Increased pumping to meet the needs of an increasing resident population has resulted in ground-water overdraft in parts of the ground-water basin. Most of the water resources of the basin are managed by the Mojave Water Agency (MWA) and the U.S. Marine Corps Air/Ground Combat Center at Twentynine Palms (USMCAGCC). To help manage the ground-water resources, the MWA and the U.S. Marine Corps, Department of the Navy, requested the U.S. Geological Survey (USGS) to construct a regional water-table map of the Morongo ground-water basin.

The purposes of this study were to construct a regional water-table map and determine areas of water-level change in the Morongo Basin. Existing data were evaluated and water levels were measured in selected wells throughout the Morongo Basin. Water-level measurements were used to construct a regional water-table map for 1994 conditions (fig. 1), and available historical water levels were used to construct hydrographs (shown in fig. 1) and determine water-level change at selected wells.

Results of this study will aid the USGS in evaluating its current ground-water monitoring network in the Morongo Basin. In addition, information gained through this study will contribute to ongoing projects in the area, such as the Regional Aquifer-System Analysis (RASA) of Southern California.

Acknowledgments

Several local water agencies contributed water-level data used in this report. Those agencies include the Bighorn-Desert View Water Agency in Landers, the Hi-Desert Water District in Yucca Valley, the Joshua Basin Water District in Joshua Tree, and the Twentynine Palms Water District in Twentynine Palms. In addition, the results of studies at the USMCAGCC by Jacobs Engineering were very helpful to this study.

Description of Study Area

As defined for this study, the 1,000-square-mile Morongo ground-water basin consists of several alluvium-filled valleys and basins that are surrounded by the San Bernardino Mountains on the west, the Ord and Granite Mountains on the north, the Bullion Mountains on the east, and the Pinto and Little San Bernardino Mountains on the south. (Generally, the lightest and darkest gray areas of the shaded-relief map represent higher topography.) Previous investigators divided the Morongo Basin area into 17 or more separate ground-water basins or subbasins, including the Lucerne, Fry, Johnson, Upper Johnson, Means, Pipes, Reche, Warren, Copper Mountain, Joshua Tree, Giant Rock, Emerson, Surprise Spring, Mesquite, Deadman, Twentynine Palms, and Mainside Basins (fig. 2). The ground-water-basin boundaries shown in figure 2 are defined by faults, low-permeability rocks, and other ground-water barriers that generally restrict ground-water movement in the study area.

The climate of the Morongo Basin is typical of the Mojave Desert. The area receives little precipitation, and recharge to ground water is minimal. Average annual precipitation on the basin floor ranges from 4 to 6 in. (Rantz, 1969). Recently, MWA has begun an artificial-recharge project in Yucca Valley (Warren Basin) and is planning an artificial-recharge project near Lucerne Valley (Lucerne Basin). Local water districts, municipalities, the USMCAGCC, and private well owners rely on the local ground water for municipal, domestic, and agricultural needs.

The basin is largely undeveloped desert except for the towns of Lucerne Valley, Yucca Valley, Joshua Tree, Landers, and Twentynine Palms, and the main facility (Mainside) at the USMCAGCC. Agricultural development in the basin, with the exception of Lucerne Valley, is minimal.

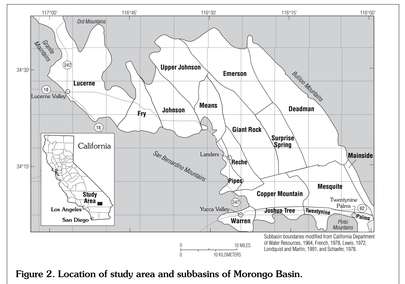


Figure 2. Location of study area and subbasins of Morongo Basin.

Geohydrology

Non-water-bearing igneous and metamorphic rocks underlie the ground-water basin and form the mountains and hills that surround the basin. These rocks contain virtually no water except where they are jointed or fractured.

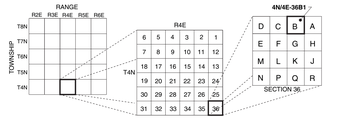
Alluvial deposits of Quaternary and Tertiary age fill the Morongo ground-water basin to a maximum depth of 10,000 ft near the eastern edge of the basin north of Deadman Lake (Moyle, 1984). In general, the deposits are unconsolidated at land surface and become partly consolidated with depth. The unconsolidated deposits, where saturated, are the only deposits from which significant quantities of ground water can be obtained.

The Morongo Basin is crossed by several northwest-trending faults that show evidence of both lateral and vertical movement (Bortugno, 1986). Large differences in water level across some of these faults suggest that they impede ground-water movement (F.S. Riley and G.F. Worts, Jr., USGS, written commun., 1953; Lewis, 1972; Schaefer, 1978; Londquist and Martin, 1991). The barrier effect of the faults is believed to be caused by compaction and deformation of the water-bearing deposits immediately adjacent to the faults and by cementation of the fault zone by mineral deposition (F.S. Riley and G.F. Worts, Jr., USGS, written commun., 1953; Schaefer, 1978; and Londquist and Martin, 1991). The Pinto Mountain Fault, its splays, and the mountain-front faults of the San Bernardino Mountains near Lucerne Basin are the only east-west-trending faults that have been identified in the study area. The Pinto Mountain Fault system also seems to be a barrier to ground-water movement. According to Bortugno (1986), most of the faults have been tectonically active within the Quaternary period.

Barriers to ground-water flow are also formed by the generally non-water-bearing consolidated rocks that compose the mountain ranges and the antiformal bedrock structure (transverse arch) located in the southern part of the Surprise Spring Basin.

Well-Numbering System

Wells are identified and numbered according to their location in the rectangular system for the subdivision of public lands. Identification consists of the township number, north or south; the range number, east or west; and the section number. Each section is divided into sixteen 40-acre tracts lettered consecutively (except I and O), beginning with A in the northeast corner of the section and progressing in a sinusoidal manner to R in the southeast corner. Within the 40-acre tract, wells are sequentially numbered in the order they are inventoried. The final letter refers to the base line and meridian. In California, there are three base lines and meridians; Humboldt (H), Mount Diablo (M), and San Bernardino (S). All wells in the study area are referenced to the San Bernardino base line and meridian (S). Well numbers consist of 15 characters and follow the format 004N004E36B01S. In this report, well numbers are abbreviated and written 4N/4E-36B1. Wells in the same township and range are referred to by only their section designation, 36B1. The following diagram shows how the number for well 4N/4E-36B1 is derived.



Well-numbering diagram

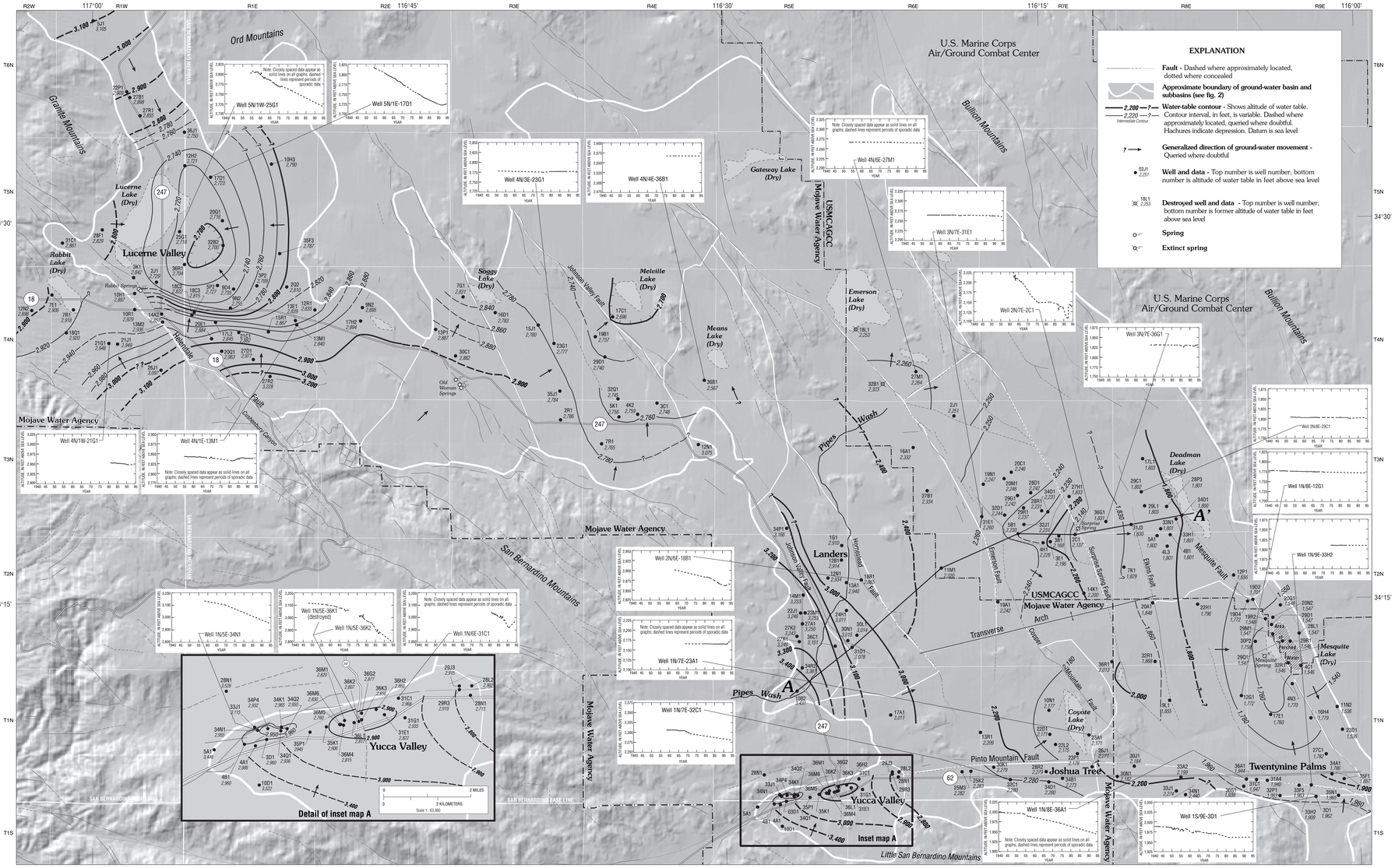
Conversion Factors

Multiply	By	To obtain
foot (ft)	0.3048	meter
foot per year (ft/yr)	0.3048	meter per year
inch (in.)	25.4	millimeter
mile (mi)	1.609	kilometer
square mile (mi^2)	2.590	square kilometer

GROUND-WATER LEVELS AND MOVEMENT

Water-level Measurements

Water-level data for this study (table 1) were collected from 248 wells during the period January-October 1994 to define the water-table surface and the direction of ground-water movement. The water table is the surface in an unconfined aquifer at which the pressure is atmospheric, and it is defined by the levels at which water stands in wells that penetrate the water body (the zone of saturation) just far enough to hold water (Lohman and others, 1972). Additional water-level data (from 11 wells) collected prior to 1994 also were used to construct map contours where current data could not be obtained or in areas of sparse data and little water-level fluctuation. For 87 wells where static water-level measurements were difficult to obtain, water levels reported by other agencies were used. The remaining water levels were measured by USGS personnel using steel or calibrated electric tapes. Water-table altitude was calculated by subtracting the water-level measurement from the land-surface altitude (determined by leveling survey or from topographic maps). Ground-water flow is from high to low water-level altitude and is perpendicular to lines of equal water-table altitude on the map (fig. 1). Arrows shown on the map indicate the approximate direction of movement.



Base from U.S. Geological Survey digital elevation data, 1:250,000, 1987, and digital data, 1:100,000, 1981-89; Universal Transverse Mercator Projection, Zone 11. Shaded relief from 1:250,000-scale Digital Elevation Model; sun illumination from northwest at 30 degrees above horizon

Faults modified from Bortugno, 1986; Londquist and Martin, 1991; J.C. Matti, and G.I. Dixon, U.S. Geological Survey, written commun., 1994; Schaefer, 1978

Figure 1. Altitude of the water table in 1994 and water-level changes at selected wells.

GROUND-WATER LEVELS AND MOVEMENT--Continued

Ground-Water Movement

In general, the water-table map indicates that ground water flows eastward and northward from the San Bernardino Mountains. From Pipes Wash, flow is eastward toward the localized sinks in the water table at Deadman and Mesquite dry lakes. Ground water pumping by the USMCAGCC in the Surprise Spring Basin has created a ground-water depression and has locally changed the direction of ground-water movement. From Cushenbury Canyon and other washes along the northern front of the San Bernardino Mountains, flow is northeastward to the pumping depression in the Lucerne Basin, and to the Soggy, Melville, and Means dry lakes. As ground water moves eastward through the Morongo Basin, subsurface flow across faults is impeded, resulting in a steplike decrease in water levels (fig. 3). For example, there is a water-level difference of more than 300 ft across the Surprise Spring Fault, near extinct Surprise Spring. Between the faults, the hydraulic gradient is approximately constant and generally very low. The past and present occurrence of springs at fault boundaries (Rabbit Springs, Old Woman Springs, Surprise Spring, and Mesquite Spring) indicates diversion of flow to the surface across faults at these locations, and emphasizes the importance of faults in controlling ground-water movement. Ground water leaves the basin across the Mesquite Fault in the southeastern part of the basin, and ultimately moves eastward toward Dale Dry Lake (not shown) (F.S. Riley and G.F. Worts, Jr., written commun., 1953).

Other patterns indicated by the contour lines and supported by previous findings are (1) northward flow from the Little San Bernardino Mountains to the Pinto Mountain Fault (Lewis, 1972), (2) minor flow southward from the San Bernardino Mountains into Warren Basin (Lewis, 1972), and (3) southward flow into Lucerne Basin from the Ord Mountains (Schaefer, 1979). Rates of ground-water movement in areas of the basin unaffected by pumping are low—generally a few feet per year (French, 1978).

Ground-water depressions are present in the areas of highest historical and current pumpage: Warren, Lucerne, and Surprise Spring Basins. Construction of water-table contours in Warren Basin was difficult because water levels vary considerably. To show small-scale variations, the Warren Basin area (inset map A) is enlarged to 1:63,360 scale. The variability might be due to (1) the presence of faults that separate the area into small isolated compartments, and (or) (2) incomplete recovery of the water table in the public-supply wells at the time of measurement--even though pumping had ceased 24 hours prior to measurement.

Perched water occurs in the Mainside Basin (under Mesquite Dry Lake) approximately 130 ft above the regional water table. Movement of this water seems to be southeastward, similar to that of the regional ground water below. The probable source of this perched water is spreading ponds that are used for sewage-water treatment.

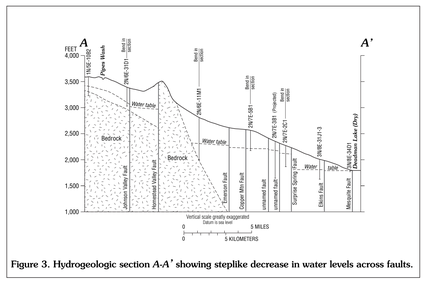


Figure 3. Hydrogeologic section *A-A'* showing steplike decrease in water levels across faults.

HISTORICAL WATER-LEVEL CHANGES

Available data for wells in the Morongo Basin were evaluated to determine water-level changes in different parts of the basin. Twenty-one long-term hydrographs for selected wells are shown on the large map. Water levels have remained relatively constant in the Deadman, Emerson, Mesquite, Mainside, Copper Mountain, Johnson, Upper Johnson, and Fry Basins, where the resident population is small and pumpage is minimal or nonexistent. Available data were insufficient to determine fluctuations of the water table in the Pipes, Emerson, or Giant Rock Basins. Water-table declines have occurred in parts of the Reche, Joshua Tree, Twentynine Palms, Surprise Spring, and Warren Basins. In the Reche Basin, the water level has declined about 36 ft since 1963 at well 2N/8E-18B1, probably the result of pumpage to supply the town of Landers; in the Joshua Tree and Twentynine Palms Basins, pumpage to supply the towns of Joshua Tree and Twentynine Palms has caused declines of about 25 ft since 1963 at well 1N/7E-32C1, and about 54 ft since 1940 at well 1N/8E-36A1; in the Surprise Spring Basin, the water level has declined 110 ft since 1960 at well 2N/7E-2C1 as a result of pumpage for the USMCAGCC; and in the Lucerne Basin, the water level has declined as much as 94 ft since 1954 at well 5N/1E-17D1, near the town of Lucerne Valley.

The largest observed water-level decline in the study area is in the Warren Basin, at Yucca Valley, where the combined decline since 1947 is 309 ft at well 1N/5E-36K1 (destroyed) and nearby well 1N/5E-36K2. The data for these two wells were combined to give a better indication of total decline in this area. In the western part of Warren Basin, the decline at well 1N/5E-34N1 is about 178 ft since 1958. These large declines probably result from increased pumpage to supply the growing population of Yucca Valley. The magnitude of those declines indicates small storage in compartments of the aquifer that are bounded by faults in combination with minimal natural recharge.

References Cited

Bortugno, E.J., 1986, Map showing recency of faulting, San Bernardino Quadrangle, California: California Division of Mines and Geology Regional Geologic Map Series, San Bernardino Quadrangle-map no. 3A, scale 1:250,000.

California Department of Water Resources, 1964, Names and areal code numbers of hydrologic areas in the Southern District: California Department of Water Resources Office Report, 57 p.

French, J.J., 1978, Ground-water storage in the Johnson Valley area, San Bernardino County, California: U.S. Geological Survey Water-Resources Investigations Report 77-130, 35 p.

Lewis, R.E., 1972, Ground-water resources of the Yucca Valley-Joshua Tree area, San Bernardino County, California: U.S. Geological Survey Open-File Report, 51 p.

Table 1. Summary of well data, Morongo Basin

[State well No.: See "Well-Numbering System" section; some numbers subject to change upon verification. USGS identification No. consists of latitude, longitude, and sequence number. Altitude of land surface and altitude of water level in feet (rounded) above sea level. Casing depth, perforations, and obstruction in feet below land surface. Measurement method: **S**, steel tape; **R**, reported by other agencies; **V**, calibrated electric tape. Well notes: **M**, USGS multiple-depth piezometer; **O**, obstruction at specified depth; **P**, public-supply well; **PW**, perched water; **Z**, destroyed well; *, data not plotted on map because of overcrowding of similar information]

State well No.	USGS identification	Date of measurement	Altitude of land surface	Depth to water	Water-level Altitude	Meas-urement method	Casing depth	Perforations Top	Perforations Bottom	Well notes
1N/5E-10R2	341139116262601	07-27-94	3,590	158.77	3,431	S	193	110	150	O at 192
1N/5E-24N1	340831115261301	05-06-94	3,635	107.45	3,528	S	155	–	–	–
1N/5E-33J1	340735116272901	05-06-94	3,171	255.87	3,115	S	310	245	310	O at 280
1N/5E-34K1	340725116264701	05-05-94	3,380	415.20	2,965	R	640	340	640	P
1N/5E-36K1	340725116270001	05-06-94	3,380	425.5	2,955	R	640	340	640	P
1N/5E-36K2	340725116270001	05-06-94	3,380	426.5	2,953	R	1,010	390	1,010	P
1N/5E-36Q2	340725116264001	05-04-94	3,360	423.7	2,936	R	757	370	571	P
1N/5E-36Q3	340725116264001	05-06-94	3,360	424.1	2,936	R	500	300	500	P
1N/5E-36Q4	340725116264001	05-06-94	3,360	426.1	2,934	R	500	300	500	P
1N/5E-36R1	340725116262701	05-05-94	3,280	335.2	2,945	R	504	194	494	P
1N/5E-36G1	340736116264201	05-05-94	3,225	346.51	2,878	V	570	550	570	*M
1N/5E-36G2	340736116264202	05-05-94	3,225	348.04	2,877	S	400	380	400	M
1N/5E-36K1	340736116264301	05-05-94	3,230	423.39	2,807	R	1,000	400	1,000	P
1N/5E-36K2	340736116264601	05-05-94	3,230	423.20	2,807	R	–	–	–	P
1N/5E-36K3	340736116264301	05-04-94	3,230	374	2,856	R	1,115	530	1,115	P
1N/5E-36L1	340736116264501	05-04-94	3,230	415.1	2,815	R	755	275	725	P
1N/5E-36M1	340737116265001	05-05-94	3,250	429.90	2,820	V	570	550	570	M
1N/5E-36M2	340737116265001	05-05-94	3,250	430.00	2,820	V	570	550	570	M
1N/5E-36M5	340737116265701	05-04-94	3,245	405.1	2,760	R	1,450	800	1,450	P
1N/5E-36M6	340737116265601	05-04-94	3,245	414.7	2,830	R	800	450	800	P
1N/6E-13R1	340953116375001	05-05-94	2,650	440.52	2,209	V	715	455	710	–
1N/6E-17A1	341003116321301	06-09-94	3,309	297.57	3,011	R	–	–	–	–
1N/6E-17M1	340839116320101	05-06-94	3,180	440.00	2,740	R	740	–	740	*P
1N/6E-25M2	340811116315601	05-30-94	2,715	444.62	2,270	R	500	452	–	*P
1N/6E-25M3	340811116315501	05-30-94	2,720	438.00	2,282	R	704	452	–	P
1N/6E-26A1	340811116311001	05-04-94	2,680	472.72	2,207	V	500	–	–	–
1N/6E-26N2	340809116311601	05-04-94	2,685	392.30	2,315	V	500	228	465	O at 212
1N/6E-29J1	340823116225901	07-29-94	3,095	180	2,915	R	803	350	773	–
1N/6E-29K1	340823116225601	07-29-94	3,105	186	2,919	R	680	360	680	P
1N/6E-32C1	340750116254401	05-05-94	3,090	230.9	2,968	R	–	–	–	P
1N/6E-32G1	340750116254201	05-05-94	3,250	315	2,935	R	–	–	–	–
1N/6E-32Q1	340750116254301	07-29-94	3,250	315	2,935	R	–	–	–	–
1N/6E-10N1	341004116144301	05-02-94	2,585	208.24	2,377	V	297	–	–	–
1N/7E-22G1	340967116414201	05-24-94	2,845	219.94	2,625	V	506	464	506	–
1N/7E-23L2	340921116415701	05-02-94	2,408	232.82	2,175	V	593	243	587	–
1N/7E-26A1	340839116405101	05-02-94	2,450	250.00	2,200	V	500	250	500	O at 230
1N/7E-27F1	340841116413601	05-03-94	2,362	203.93	2,178	V	429	–	429	–
1N/7E-29J1	340830116424201	05-30-94	2,510	239.41	2,271	R	401	277	401	P
1N/7E-29Q1	340819116421601	05-02-94	2,520	240.00	2,280	V	500	–	–	–
1N/7E-30R2	340819116405201	05-02-94	2,464	184.65	2,279	V	501	–	–	–
1N/7E-32C1	340801116395101	05-04-94	2,350	325.00	2,025	V	362	–	–	P
1N/7E-32C2	340801116395201	05-05-94	2,410	329.56	2,280	V	500	–	–	–
1N/7E-34B1	340801116410601	05-26-94	2,489	216.15	2,273	V	590	327	590	–
1N/7E-35A1	340801116425101	05-26-94	2,520	223.21	2,297	V	500	300	500	–
1N/8E-19C1	341136116405001	05-05-94	2,140	324.61	1,815	V	396	282	396	–
1N/8E-12G1	341144116405701	05-02-94	1,973	200.78	1,772	V	–	–	–	–
1N/8E-36A1	340831116360201	05-04-94	2,375	168.83	2,206	V	600	80	590	–
1N/8E-36E1	340831116354301	06-28-93	2,353	164.50	2,188	R	400	145	312	*P
1N/8E-36E2	340831116354301	05-05-94	2,353	164.50	2,188	R	400	145	312	*P
1N/8E-33A2	340904116361601	05-05-94	2,510	311.10	2,199	R	500	345	500	P
1N/8E-33A3	340903116362901	05-22-94	2,510	312.84	2,197	R	408	278	403	*P
1N/8E-33A4	340903116362901	05-27-94	2,510	307.58	2,202	R	408	318	403	*P
1N/8E-33A5	340904116362901	05-22-94	2,510	309.75	2,200	R	410	310	410	*P
1N/8E-33A6	340903116362901	05-22-94	2,510	309.75	2,200	R	410	310	410	*P
1N/8E-34M1	340721116402601	05-04-94	2,700	511.26	2,188	V	650	–	–	–
1N/8E-34N1	340721116402701	05-04-94	2,690	249.97	2,440	V	350	250	350	–
1N/8E-35A1	340721116395101	05-04-94	2,610	420.00	2,190	V	500	–	–	P
1N/8E-35G1	340721116395201	05-04-94	2,610	329.56	2,280	V	500	220	450	P
1N/8E-36H2	340721116382501	08-31-93	2,360	217.08	2,143	R	337	32	337	*P
1N/8E-36J1	340721116382601	10-11-93	2,360	223.21	2,136	R	244	218	243	–
1N/9E-04N3	341411116430901	05-03-94	1,787	16.90	1,770	V	500	390	495	–
1N/9E-05K1	341411116415601	05-03-94	1,780	19.50	1,760	V	–	–	–	–
1N/9E-08A1	341355116430401	05-03-94	1,765	15.76	1,749	V	55	–	–	–
1N/9E-17E1	341031116441401	05-02-94	1,870	109.68	1,760	V	–	–	–	–
1N/9E-23G1	340943116435501	05-27-94	1,840	263.63	1,576	V	–	–	–	–
1N/9E-27C1	340855116413601	05-03-94	1,867	84.63	1,782	V	–	–	–	–
1N/9E-29A1	340817116430101	05-03-94	1,845	135.00	1,710	V	398	160	398	P
1N/9E-31C1	340777116446501	05-04-94	2,105	158.50	1947	R	–	–	–	–
1N/9E-32P1	340749116434501	05-20-94	2,140	177.42	1,963	R	320	220	320	P
1N/9E-33P3	340749116432502	05-03-94	1,881	17.80	1,863	V	20	20	22	–
1N/9E-35B2	340741116432802	05-03-94	1,961	51.69	1,909	V	37	35	37	–
1N/9E-35H1	340741116430101	05-03-94	1,945	57.50	1,887	V	57	55	57	–
1N/9E-35K5	340741116432804	05-03-94	1,973	23.33	1,950	V	28	26	28	*
1N/9E-36A1	340806116412101	05-03-94	1,938	151.93	1,786	V	–	–	–	–
1N/9E-36H1	340736116412101	05-03-94	1,966	165.50	1,800	V	–	–	–	–
1N/9E-19N1	340734116402601	05-04-94	2,180	315.62	1,865	V	398	147	347	–
1N/9E-02D1	340711116271001	01-06-94	3,340	380.52	2,960	R	940	600	940	P
1N/9E-04A1	340708116272301	04-26-94	3,310	345.10	2,965	R	325	200	325	P
1N/9E-04B1	340708116272401	04-26-94	3,339	379.22	2,960	R	–	–	–	–
1N/9E-05A1	340708116270101	05-04-94	3,350	360.00	2,990	V	390	145	340	–
1N/9E-05B1	340641116272201	05-06-94	3,376	47.69	3,328	V	130	–	–	–
1N/9E-05D1	340714116270701	05-04-94	2,075	113.32	1,962	S	275	–	–	–
2N/9E-01G1	341716116262901	05-25-94	3,010	100.42	2,910	R	–	–	–	–
2N/9E-12B1	341643116331101	06-09-94	3,059	145.17	2,914	R	–	–	–	P
2N/9E-12H1	341643116324101	06-09-94	3,080	150.00	2,930	R	–	–	–	P
2N/9E-12N2	341604116324601	05-25-94	3,217	283.53	2,934	V	358	337	358	–
2N/9E-13A1	341605116341601	05-26-94	3,079	138.90	2,940	V	190	135	190	O at 155
2N/9E-14B1	341605116323601	05-26-94	3,422	490.03	2,933	V	505	270	505	–
2N/9E-22D1	341438116326201	06-09-94	3,303	257	3,246	R	365	130	775	P
2N/9E-23A1	341438116335101	06-09-94	3,280	270.00	3,010	R	500	270	500	P
2N/9E-24H1	341414116343701	06-09-94	3,262	270.99	2,991	R	310	290	310	M
2N/9E-27A1	341412116362301	05-05-94	3,470	219.76	3,250	S	485	443	485	O at 443
2N/9E-27B1	341412116362101	05-05-94	3,470	219.76	3,250	S	322	314	319	P
2N/9E-27K3	341331116362601	06-09-94	3,468	224.85	3,243	R	500	–	–	–
2N/9E-27R1	341331116362301	06-09-94	3,470	221.08	3,249	R	475	260	470	P
2N/9E-30A1	341331116343101	05-26-94	3,600	163.29	3,437	V	–	–	–	–
2N/9E-30C1	341331116344901	06-09-94	3,433	282.33	3,151	R	–	–	–	–
2N/9E-30H1	341331116343001	05-26-94	3,430	280.00	3,150	V	790	790	–	–
2N/9E-03B1	341050116362101	05-26-94	3,087	221.99	2,865	V	310	187	310	P
2N/9E-30L1	341303116324901	05-05-94	3,330	316.41	3,014	S	377	123	375	O at 350
2N/9E-32N1	341213116343101	06-09-94	3,366	351.08	3,015	S	920	380	920	–
2N/9E-35D1	341134116345501	05-05-94	3,395	316.49	3,078	S	358	337	358	–
2N/9E-36A1	341134116362101	05-05-94	3,380	320.00	3,060	V	500	320	500	O at 325
2N/9E-02G1	341716116321701	05-23-94	3,294	180.79	3,114	V	525	250	512	*P
2N/9E-03A1	341716116316201	05-23-94	3,301	160.54	3,140	V	560	140	540	*M
2N/9E-03H1	341716116315201	05-23-94	3,300	209.67	3,090	V	500	200	500	P
2N/9E-04C1	341649116315401	05-23-94	3,383	188.83	3,196	V	510	230	510	P
2N/9E-04D1	341649116315101	05-23-94	3,380	189.00	3,191	V	500	230	500	P
2N/9E-05A1	341649116321101	05-23-94	3,340	167.00	3,173	V	460	165	460	P
2N/9E-08A1	341717116305501	05-01-94	3,280	201.85	3,078	V	447	165	445	–
2N/9E-08B1	341717116305701	05-01-94	3,280	201.85	3,078	V	447	165	445	–
2N/9E-08R1	341717116285701	05-01-94	2,905	204.41	2,801	R	227	32	227	–
2N/9E-09A1	341717116290101	05-01-94	2,904	208.16	2,695	R	226	202	226	–
2N/9E-09B3	341717116285901	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09D1	341717116285601	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09E1	341717116290201	05-09-94	2,925	224.01	1,801	R	246	221	246	*
2N/9E-09E2	341717116290201	05-06-94	2,925	224.01	1,801	R	246	221	246	*
2N/9E-09F1	341717116285301	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09F2	341717116285301	05-05-94	2,925	227.59	1,801	R	248	225	248	*
2N/9E-09F3	341717116285301	07-20-94	2,922	221.05	1,801	R	240	215	240	*
2N/9E-09G1	341717116290401	05-05-94	2,925	224.01	1,801	R	246	221	246	*
2N/9E-09H1	341717116290401	05-06-94	2,925	224.01	1,801	R	246	221	246	*
2N/9E-09J1	341717116285101	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09K1	341717116285101	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09L1	341717116290601	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09M1	341717116290601	05-06-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09N1	341717116285001	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09P1	341717116290001	05-06-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09Q1	341717116290001	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09R1	341717116285001	05-05-94	2,910	209.28	1,801	R	230	204	229	*
2N/9E-09R2	341717116285001	07-20-